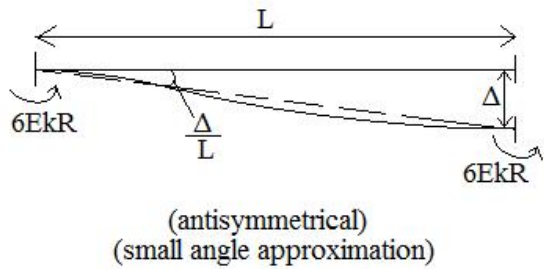


Treatment of joint translations



If there are joint translations, then

$$M_{ja} = DM_{ja} + COM_{ja} + FEM_{ja}$$

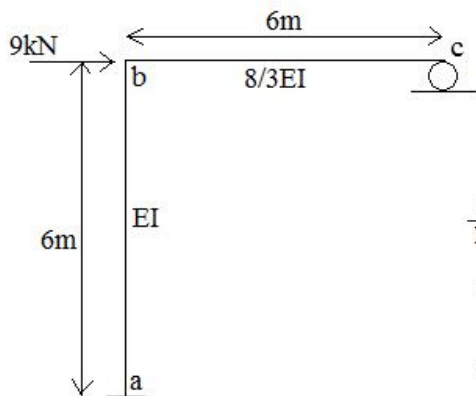
+ additional joint translation moment

relative displacement, shown, results in negative moment, shown

$$R = \frac{\Delta}{L}$$

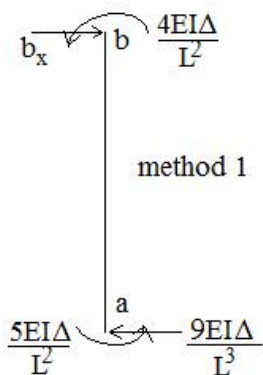
e.g. 1

e.g. 1



$$\frac{(8/3)I}{6} \left(\frac{3}{4} \right) = k_{bc}' \quad \frac{I}{6} = k_{ba}'$$

| | ab | ba | bc | cb |
|------------------------|--------------------------|--------------------------|-------------------------|----|
| $\frac{k'}{\Sigma k'}$ | 0 | 1/3 | 2/3 | 1 |
| FEM | $\frac{-6EI\Delta}{L^2}$ | $\frac{-6EI\Delta}{L^2}$ | | |
| DM | | $\frac{2EI\Delta}{L^2}$ | $\frac{4EI\Delta}{L^2}$ | |
| COM | $\frac{EI\Delta}{L^2}$ | | | |
| Σ | $\frac{-5EI\Delta}{L^2}$ | $\frac{-4EI\Delta}{L^2}$ | $\frac{4EI\Delta}{L^2}$ | 0 |



$$\frac{9EI\Delta}{L^3} \text{ from } \Sigma M_b = 0 \text{ for member ab}$$

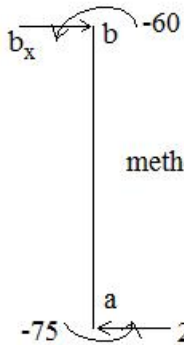
$$\text{From } \Sigma F_x = 0 \text{ for the whole frame, } \frac{9EI\Delta}{L^3} = 9 \Rightarrow \Delta = \frac{L^3}{EI}$$

$$\Rightarrow M_{ab} = -30kN \cdot m \quad M_{ba} = -24kN \cdot m \quad M_{bc} = 24kN \cdot m$$

OR

Choose arbitrary FEM = -90 kN*m

| | <u>ab</u> | <u>ba</u> | <u>bc</u> | <u>cb</u> |
|----------|-----------|-----------------|-----------------|-----------------|
| FEM | -90 | -90 | | |
| DM | | 30 | 60 | |
| COM | <u>15</u> | <u> </u> | <u> </u> | <u> </u> |
| Σ | -75 | -60 | 60 | 0 |



22.5 from $\Sigma M_b = 0$ for member ab

method 2

From $\Sigma F_x = 0$ for the whole frame, $22.5 \neq 9$

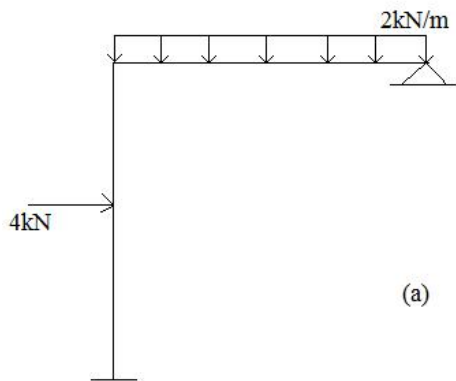
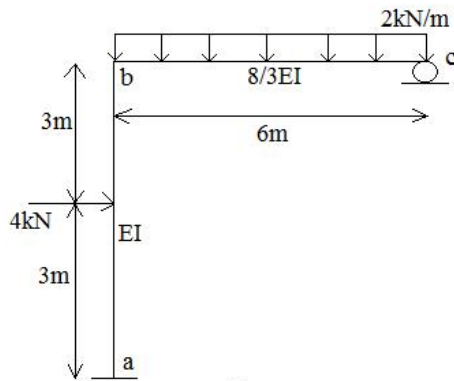
Need correction factor of $9/22.5$ for all forces and moments

$$\Rightarrow M_{ab} = -30 \text{ kN} \cdot \text{m} \quad M_{ba} = -24 \text{ kN} \cdot \text{m} \quad M_{bc} = 24 \text{ kN} \cdot \text{m}$$

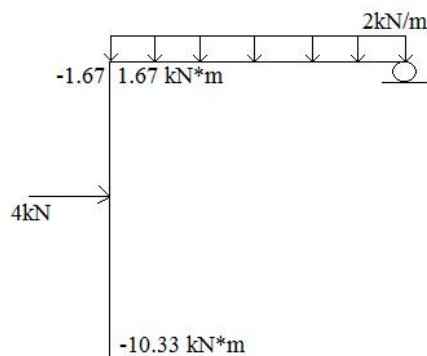
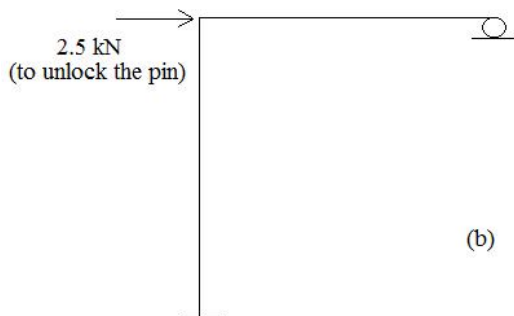
note: method 2 does not even use the formula $M = -6EkR$. Since the solutions for method 1 and 2 match correctly, we know our derivation for $M = -6EkR$ is correct.

Method 2 is more manageable, but how can we use method 2 if the loads are not only located at the joints?

e.g. 2



+



(a)

| | <u>ab</u> | <u>ba</u> | <u>bc</u> | <u>cb</u> |
|------------------------|-----------|-----------|-----------|-----------|
| $\frac{k'}{\Sigma k'}$ | 0 | 1/3 | 2/3 | 1 |
| FEM | -3 | 3 | -6 | 6 |
| DM | | 1 | 2 | -6 |
| COM | .5 | | -3 | |
| DM | | 1 | 2 | |
| COM | .5 | | | |
| Σ | -2 | 5 | -5 | 0 |

From $\Sigma F_x = 0$ for the whole frame, the pin has a reaction of 2.5kN acting left. This must be counter-acted as shown in (b) since the beam does not have a pin.

(from ΣM_b for member ab)

(b)

| | <u>ab</u> | <u>ba</u> | <u>bc</u> | <u>cb</u> |
|----------|-----------|-----------|-----------|-----------|
| FEM | -90 | -90 | | |
| DM | | 30 | 60 | |
| COM | 15 | | | |
| Σ | -75 | -60 | 60 | 0 |

From $\Sigma M_b = 0$ for member ab and $\Sigma F_x = 0$ for the whole frame, the correction factor is $2.5/22.5$, where 22.5 is from the previous example. So, moments for b:

| <u>ab</u> | <u>ba</u> | <u>bc</u> | <u>cb</u> |
|-----------|-----------|-----------|-----------|
| -8.33 | -6.67 | 6.67 | 0 |

$$(a) + (b) \Rightarrow M_{ab} = -10.33 \quad M_{ba} = -1.67 \quad M_{bc} = 1.67 \text{ kN} \cdot \text{m}$$

note: moment distribution can be used to find moments that include the effect of sway for asymmetrical vertical loadings, and for multi-story frames, but it quickly becomes cumbersome to do by hand.

Works Cited

Hsieh, Yuan-Yu, and S.T. Mau. Elementary Theory of Structures: Fourth Edition. Prentice Hall. Upper Saddle River, NJ 1995.
 Trifunac, Mihailo. Lecturer. University of Southern California. CE358. Fall 2005.